- (21) Ginnings, D. C., Corruccini, R. L., Ind. Eng. Chem. 40, 1990 (1948).
- (22) Haltenberger, W., Jr., Ibid., 31, 783 (1939).
- (23) Hedström, B. O. A., Tjus, E., Chem.-Ing.-Tech. 24, 22 (1952).
- (24) Hougen, O. A., Watson, K. M., "Chemical Process Principles," p. 495, Wiley, New York, 1947. (25) Hougen, O. A., Watson, K. M., Ragatz, R. A., "Chemical
- Process Principles," p. 324, Wiley, New York, 1954.
- (26) Ibid., p. 325.
- (27) Ibid., p. 326.
- (28) Ibid., p. 327.
- (29) Ibid., p. 390. (30) International Critical Tables, vol. 4, p. 262, McGraw-Hill, New York, 1928.
- (31) Ibid., vol. 5, p. 102.
- (32) Ibid., p. 114
- (33) Ibid., p. 132.
- (34) Ibid., p. 137.
- (35) Ibid., p. 138.
- (36) Ibid., p. 159.
- (37) Keenan, J. H., Keyes, F. G., "Thermodynamic Properties of Steam," Wiley, New York, 1936.
- (38) Kendall, J., Booge, J. E., Andrews, J. C., J. Am. Chem. Soc. 39, 2303 (1917).
- (39) Kobe, K. A., Couch, E. J., Jr., Ind. Eng. Chem. 46, 377 (1954).
- (40) Kobe, K. A., Harrison, R. H., and Pennington, R. E., Petroleum Refiner 30, No. 8, 119 (1951).
- (41) Lange, N. A., "Handbook of Chemistry," 7th ed., Handbook Publishers, Sandusky, Ohio, 1949.
- (42) Levy, B., Davis, T. W., J. Am. Chem. Soc. 76, 3268 (1954).

- (43) McKinley, C., Brown, G. G., Chem. Met. Eng. 49, No. 5, 142 (1942)
- (44) Merkel, F., Arch. Warmewirtsch. u. Dampikesselw. 10, 13 (1929).
- (45) Merkel, F., Z. Ver. deut. Ing. 72, 109 (1928).
- (46) Newmann, M. B., Z. physik. Chem. A158, 285 (1932). (47) Othmer, D. F., Silvis, S. J., Spiel, A., Ind. Eng. Chem. 44,
- 1864 (1952). (48) Parks, G. S., Kelley, K. K., J. Am. Chem. Soc. 47, 2089 (1925).
- (49) Parks, G. S., Nelson, W. K., J. Phys. Chem. 32, 61 (1928).
  (50) Perry, J. H., "Chemical Engineers' Handbook," 3rd ed., p. 1052, McGraw-Hill, New York, 1950.
- (51) Ibid., p. 1701.
- (52) Plewes, A. C., others, Can. J. Technol. 32, 133 (1954).
- (53) Ross, W. D., Chem. Eng. Progr. 48, 314 (1952).
- (54) Schiebl, K., "Wärmewirtschaft in der Zuckerindustrie," p. 166 and appended chart, Steinkopf, Dresden, 1939.
- (55) Senter, G., Proc. Chem. Soc. (London) 25, 292 (1909).
- (56) Standiford, F. C., Badger, W. L., Ind. Eng. Chem. 46, 2400 (1954).
- (57) Tyner, M., A.I.Ch.E. Journal 1, 87 (1955).
- (58) Tyner, M., Chem. Eng. Progr. 45, 49 (1950).
- (59) Van Nuys, C. C., Trans. Am. Inst. Chem. Engrs. 39, 663 (1943)
- (60) Vogt, E. G., Ibid., 43, 39 (1947).
- (61) Wilson, A., Simons, E. L., Ind. Eng. Chem. 44, 2214 (1952). (62) Wilson, H. R., McCabe, W. L., Ibid., 34, 558 (1942).

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# Liquid-Liquid Equilibria for Alcohol -Sodium Hydroxide-Water Systems

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 ${f S}$  olubility data have been published for sodium hydroxide in aqueous ethyl alcohol (2) and in aqueous isobutyl alcohol (1), but no data were available for aqueous isopropyl alcohol (I.P.A.). Information on the solubility of strong caustic soda solutions in isopropyl alcohol and in industrial methylated spirit (I.M.S.) was required for pilot plant neutralization experiments. Industrial methylated spirit is the commercial form of ethyl alcohol available in the United Kingdom.

On refining petroleum, particularly on processing for highly refined white oils by sulfonation, it is necessary to extract oil-soluble sulfonic acids from the sulfonated oil and to neutralize to the corresponding sodium salts. The quality and especially the color of the by-product sodium petroleum sulfonates are influenced by the residence time of the sulfonic acid-oil reaction product, particularly if the equipment is mild steel. For the two systems of processing which may be applied-centrifuge or batch-it is essential that, for the centrifuge process, neutralization and extraction proceed simultaneously, whereas for batch

processing it is preferred that the two stages should take place concurrently. For either processing system, it is a distinct advantage if a homogeneous neutralizing-extracting solution is used.

Preliminary experiments indicated that industrial methylated spirit and ethyl alcohol behave differently and it was decided therefore to investigate the systems for industrial methylated spirit and isopropyl alcohol at 25° and 60°C.

#### MATERIALS

As it was expected that information resulting from this project might be applied to plant scale processing, no attempt was made to purify materials which were of technical quality and had the following properties.

	Specific Gravity at 20 °C.	Strength, Weight %
Aqueous caustic soda	1.4590	43.0
I.M.S.	0.8064	94.2
I.P.A.	0.7852	100.0

	Table i. Sodium Weigh	Solubil Hydroxi It at 25°	ity Da de-Wa and 6	ta for Isoprop iter System (F 0°C. Figure:	oyl Alcoh Per Cent s 1 and 4	ol- by l)	
LP.A.	NaOH	н.(	2	I.P.A.	NaOl	н.	0
		•	Data a	at 25 °C.		•	
97.2	1 2	1	6	30.9	43	64	
87.1	0.4	12.	5	21.8	5.8	72	.4
75.1	0.4	24.	5	13.4	7.8	78	. 8
63.1	1.0	35.	9	5,8	11.7	82	.5
51.5	2.0	46.	5	2.3	18.2	79	. 5
41.1	2.7	56.	2	0.0	50,0	50	0.0(1)
Tie I	Tie Lines, Water Layer Tie Lines, So			es, Solv	ent Lay	/er	
0,6	31.5	67.	9	97.4	0.6	2	2.0
1.5	23.7	74.	8	97.2	0.6	2	2.2
Data at 60 $^{\circ}$ C.							
96.3	1.6	2.	1	31.2	3, 2	65	5.6
74.3	0.6	25.	1	21.9	4.8	73	3.3
62.5	1.0	36.	5	13.5	6.7	79	9.8
51.7	1.4	46.	9	5.9	10.6	83	8.5
40.9	2.4	56.	7	1.5	16.6	81	.9
36.0	2.8	61.	2	0.0	63.5	36	5.5(3)
Tie I	Lines, Wat	er Layer		Tie Li	nes, Solv	ent Lag	yer
0.7	30.5	68.	8	98.8	0.2	1	.0
1.3	23.4	75.	3	97.0	0.6	2	2.4
Tab	ole II. Solu Sodium Weigh	ubility D Hydroxi t at 25°	ata fo de∽₩a and 6	r Industrial N ter System (P 0°C. Figures	ethylate er Cent i 1 and 3	d Spirit by )	-
I. M. S.	NaOH	H₂C	)	I. M. S.	NaOH	H <sub>2</sub>	0
			Data a	at 25 °C.			
51.0	21.1	27.9	)	17.1	22.0	60	.9
49.2	18.9	31.9	)	11.8	23.1	65	.1
43.7	18.4	37.9	)	7.1	24.6	68	.3
37.1	18.6	44.3	3	2.9	27.6	69	.5
29.6	19.7	50.7	7	1.2	30.2	68	. 6
23.0	20.8	56.2	2	0.0	50.0	50	.0(1)
Tie L	ines, Wate	er Layer		Tie Lin	es, Solv	ent Lay	er
1.9	29.0	69.1		50.5	20.4	29	.1
0.8	34.4	64.8	5	50.7	21.0	28	. 3
Data at $60$ °C.							
60.7	16.9	22.4	•	27.1	16.4	56	.5
60.3	13.4	26.3	3	19.8	18.2	62	.0
54.3	12.2	33.5	5	13.6	19.8	66	i.6
45.3	12.9	41.8	3	7.8	22.5	69	. 7
35.6	14.7	49.7	,	3.1	26.2	70	.7
30.0	15.8	54.2	2	0.0	63.5	36	. 5 (3)
Tie L	Lines, Wate	er Layer		Tie Lin	es, Solv	ent Lay	er
1.2	31.1	67.7	,	60.1	13.5	26	.4
0.5	36.1	63.4	ł	60.8	16.6	22	.6
	Table III	. Solubi	lity D	ata for Isobut	yl Alcoh	ol -	
	Sodium	Hydroxic	le-Wat	er System (1)	) (Per Ce 2)	ent	
Icobut.	1 Alcohol	ਹਨ ਜerd N∘⊖ਸ	ਸਾ <b>ਯਾ∡</b> ਸ∩		≠7 Micobol	№аОн	H.O
-sobury	2 0	1 1	5.0	1300utyt /		67	00.0
9	5.0 6.2	1 2	025	3.1		145	84 A
	5.2	2.3	94.3	0.5	, l	21 7	770
	3.2 A 5	2.0	92.0	0.4	r	21.1	67 0
	7.J 25	5.9	91.0 00 7	0.1		50.0	50 0
		J. 8	90.7		, Timo- S		30.0 T ava-
	iie Lines,	, water 1	Jayer	1 1e	Lines, S	orvent	Layer
1	0.1	35.0	04.9 74 9	99.5	, ,	0.3	0.2
		27.0	/ 4.0	99.3	,	0.5	0.2

## PROCEDURE

The ternary diagrams for sodium hydroxide and water with industrial methylated spirit and isopropyl alcohol were constructed at 25  $^{\circ}$  and 60  $^{\circ}$ C.; the cloud point method was used to determine the boundary of the two-layer region. Tie lines were constructed by preparing mixtures of known composition, shaking them thoroughly, and separating them after equilibrium was established. The separated layers



were analyzed for sodium hydroxide content by titration with standard acid and for alcohol content by oxidation with standard potassium dichromate and iodometric determination of the excess reagent with potassium iodide and sodium thiosulfate. Water contents were determined by difference. All data were recalculated to solid sodium hydroxide content, so that they would be clearer and more precise in meaning.





Figure 3. Ternary diagrams for industrial methylated spiritsodium hydroxide-water system Per cent by weight ot 25° and 60°C. --- Tie lines at 60°C.

## RESULTS

The data for the four systems are given in Tables I to IV. Data for ethyl alcohol, industrial methylated spirit, and isopropyl alcohol at 60  $^{\circ}$ C. are shown on triangular coordinates in Figure 1; data for isobutyl alcohol, industrial methylated spirit, and isopropyl alcohol at 25  $^{\circ}$ C. are shown in Figure 2. Figures 3 and 4 compare data at 25  $^{\circ}$ 



Figure 4. Ternary diagrams for isopropyl alcohalsodium hydroxide-water system Per cent by weight ot 25° and 60°C. --- Tie lines at 60°C.

Table IV. Solubility Data for Ethyl Alcohol- Sadium Hydraxide-Water System (2) (Per Cent by Weight at 60°C. Figure 1)							
EtOH	NaOH	H <sub>2</sub> O	EtOH	NaOH	H2O		
64.1	15.4	20.5ª	0.0	63.5	36.5 ( <i>3</i> )		
Tie L	ines, Water	Layer	Tie Lir	ies, Solven	t Layer		
0.0	44.5	55.5	64.2	22.4	13.4		
1.8	34.8	63.4	65.2	13.7	21.1		
5.2	26.4	68.4	62.5	9.5	28.0		
10.0	23.3	66.7	54.1	10.2	35.7		
<sup>a</sup> This	work.						

and  $60\,^{\circ}$ C. for industrial methylated spirit and isopropyl alcohol, respectively.

#### DISCUSSION

Sodium hydroxide is considerably less soluble in isopropyl and isobutyl alcohols than in ethyl alcohol, the zones of immiscibility increasing with increasing molecular weight of alcohol. It would be interesting to compare these results with those obtained for *n*-propyl and *n*-butyl alcohols. The zones of immiscibility increase for both industrial methylated spirit and isopropyl alcohol with increasing temperature, confirming the findings of Peyronel (2) who observed similar behavior with ethyl alcohol, and suggested that rupture of the ethyl alcohol-sodium hydroxide association is greatly affected by temperature. The phenomenon is not so apparent with isopropyl alcohol and would probably be even less so with isobutyl alcohol. The concavity on the water-isobutyl alcohol side of the triangular graph, observed by Fritzsche and Stockton (1) was found with isopropyl alcohol.

Sodium hydroxide is more soluble in industrial methylated spirit than ethyl alcohol at high alcohol concentrations but at concentrations below 48% (by weight) of alcohol the solubility is reversed, probably again because of different molecular associations.

The graphs and data may be advantageously used where neutralizing blends of sodium hydroxide in alcohol are required, particularly in the petroleum industry where simultaneous neutralization and extraction of sulfonic acids may be effected. Blend proportions and concentrations to provide completely miscible neutralizing solutions may be deduced and are particularly important in centrifugal separations.

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### LITERATURE CITED

- (1) Fritzsche, R. H., Stockton, D. L., Ind. Eng. Chem. 38, 737-40 (1946).
- (2) Peyronel, G., Gazz. chim. ital. 79, 792-9 (1949).
- (3) Seidell, A., "Solubilities of Inorganic and Metal Organic Compounds," Vol. 1, p. 1284, Van Nostrand, New York, 1940.

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